Announcements

- Course website: https://coursys.sfu.ca/2019fa-cmpt-419-x1/pages/
- Instructor office hours, TASC 1 8225
 - This week: 13:00 14:30
 - In the future: Mondays 14:00 15:30
- TA (Shubam Sachdeva) office hours, ASB 9808
 - Thursdays 12:00 13:00





Linear Systems

CMPT 419/983

09/09/19





References for Linear Systems

- F. Callier & C. A. Desoer, Linear System Theory, Springer-Verlag, 1991.
- W. J. Rugh, Linear System Theory, Prentice-Hall, 1996.

Differential Equations

- Continuous time model of robotic systems
 - In general, nonlinear systems
 - One may construct discrete time models from continuous time models
- Dynamics: $\dot{x} = f(t, x, u, d), x \in \mathbb{R}^n, t \ge t_0$
 - Specifies how the robot state or configuration changes over time
 - In some ways, the most "natural" model, since $F = ma = m\ddot{x}$
 - Defining $x_1 = x, x_2 = \dot{x}$, we have

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ F \\ \hline m \end{bmatrix}$$



Differential Equations

- State: $x(t) \in \mathbb{R}^n$, $x(t_0) = x_0$
 - Contains all information needed to specify the configuration of the robot
 - Most common: position, velocity, angular position, angular velocity
- Control: $u(t) \in \mathcal{U}$
 - Examples: steering, accelerating, decelerating
 - Usually constrained to be within some set
- Disturbance: $d(t) \in \mathcal{D}$
 - Examples: wind, input noise, another agent



Linear Systems

- Differential equations generally do not have closed-form solutions
 - Numerical methods can be used to obtain approximate solutions
 - Other analysis techniques offer insight into the solutions
- Linear time-invariant (LTI) systems: $\dot{x} = Ax + Bu$
 - Damped mass spring systems
 - Circuits involving resistors, capacitors, inductors
 - Approximations of nonlinear systems





Linear Systems





(If flying near hover, and slowly) Bouffard, 2012

Road Map

- Basic properties and closed form solution
- Stability
- Linear state feedback control

LTI Systems

• Linear time-invariant (LTI) systems: $\dot{x} = Ax + Bu$



LTI Systems: Closed Form Solution

•
$$\dot{x} = Ax + Bu$$
, $x(0) = x_0$
• $x(t) = e^{At}x_0 + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau$
Matlab: expm $e^{At} = I + \frac{At}{1!} + \frac{A^2t^2}{2!} + \cdots$

Solution to LTI System: Proof

• If $\dot{x} = Ax + Bu$, $x(0) = x_0$, then $x(t) = e^{At}x_0 + \int_0^t e^{A(t-\tau)}Bu(\tau)d\tau$

• Initial conditions:
•
$$x(0) = e^{A(0)}x_0 + \int_0^0 e^{A(t-\tau)}Bu(\tau)d\tau = x_0$$

• Differentiate:
• $\dot{x} = \frac{d}{dt}(e^{At}x_0) + \frac{d}{dt}(\int_0^t e^{A(t-\tau)}Bu(\tau)d\tau)$
• $\dot{x} = Ae^{At}x_0 + A\int_0^t e^{A(t-\tau)}Bu(\tau)d\tau + Bu(t)$
• $\dot{x} = Ax(t) + Bu(t)$
 $= A\int_0^t e^{A(t-\tau)}Bu(\tau)d\tau + Bu(t)$
 $= A\int_0^t e^{A(t-\tau)}Bu(\tau)d\tau + Bu(t)$

Matrix Exponential Properties

- If $\dot{x} = Ax$, $x(0) = x_0$, then $x(t) = e^{At}x_0$ • $e^0 = I$ (follows from the above)
- $e^{A(t+s)} = e^{At}e^{As}$ • $x(t+s) = e^{A(t+s)}x_0 = e^{At}e^{As}x_0$ (A+B)t At Bt is a set of x
- $e^{(A+B)t} = e^{At}e^{Bt}$ if and only if AB = BA
- $(e^{At})^{-1} = e^{-At}$ • So $e^{At}e^{-At} = I$

•
$$\frac{d}{dt}e^{At} = Ae^{At} = e^{At}A$$

• From definition:
$$e^{At} = I + \frac{At}{1!} + \frac{A^2t^2}{2!} + \cdots$$

 e^{At} "propagates" a state forward by a duration of t, according to the system dynamics A

State transition matrix





- Equilibrium point of $\dot{x} = f(x)$ is where f(x) = 0
 - For $\dot{x} = Ax$, in general $\mathbf{0}_n$ is an equilibrium point: $x_e = 0_n$
 - Also, $x_e \in$ the nullspace of A
- Stable: x(t) is bounded for all $t \ge 0$, for all initial conditions x_0
- Asymptotically stable: $x(t) \rightarrow x_e$ as $t \rightarrow \infty$
- **Exponentially stable**: $\exists M, \alpha > 0$ such that $||x(t)|| \le Me^{-\alpha t} ||x_0||$
- The system $\dot{x} = Ax$ is exponentially stable if and only if all eigenvalues of A are in the *open* left half plane, i.e. $\forall k$, $\operatorname{Re}(\lambda_k) < 0$



Eigenvalues and Eigenvectors

- Eigenvalues:
 - If there is some vector e and scalar λ such that $Ae = \lambda e$, then e is called the eigenvector corresponding to eigenvalue λ of the matrix A

• Example:
$$A = \begin{bmatrix} 3 & 0 \\ 0 & 2 \end{bmatrix}$$

• $\begin{bmatrix} 3 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 3 \\ 0 \end{bmatrix} = 3 \begin{bmatrix} 1 \\ 0 \end{bmatrix}$
• $\begin{bmatrix} 3 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \end{bmatrix} = 2 \begin{bmatrix} 0 \\ 1 \end{bmatrix}$ \rightarrow

• When a matrix is applied to eigenvectors, the effect is simple!

Eigenvalues and Eigenvectors

• Define $T^{-1} = [e_1 \ e_2 \ \cdots \ e_n]$

• Then,
$$AT^{-1} = T^{-1}\Lambda$$
, where $\Lambda = \begin{bmatrix} \lambda_1 & & \\ & \lambda_2 & \\ & & \ddots & \\ & & & & \lambda_n \end{bmatrix}$

- $A = T^{-1}\Lambda T$. This is a **similarity transform**.
- Define z = Tx, and we have $Ax = T^{-1}\Lambda Tx = T^{-1}\Lambda z$
 - In the coordinate system obtained from applying transformation T, the map A is diagonal
 - To obtain the result of applying A in the original coordinate system, transform back with T^{-1}

Obtaining Eigenvalues and Eigenvectors

- Hand calculation: $A = \begin{bmatrix} 2 & -3 \\ -3 & 2 \end{bmatrix}$
 - Eigenvalues $Ae = \lambda e$ $Ae - \lambda Ie = 0$ $(A - \lambda I)e = 0$ Solve for λ in det $(A - \lambda I) = 0$ det $\left(\begin{bmatrix} 2 - \lambda & -3 \\ -3 & 2 - \lambda \end{bmatrix}\right) = (2 - \lambda)(2 - \lambda) - 9 = 0$ $2 - \lambda = \pm 3$

This means the matrix $A - \lambda I$ has an eigenvalue of 0

• Eigenvectors

$$\lambda = -1: \begin{bmatrix} 3 & -3 \\ -3 & 3 \end{bmatrix} e = 0 \Rightarrow e = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \qquad \qquad \lambda = 5: \begin{bmatrix} -3 & -3 \\ -3 & -3 \end{bmatrix} e = 0 \Rightarrow e = \begin{bmatrix} 1 \\ -1 \end{bmatrix}$$

 $\lambda = 2 + 3 = -1.5$

Matlab: eig(A)

Jordan Form

• Not all matrices are diagonalizable

 $\begin{array}{ll} Ae_1 = \lambda e_1 & Av_1 = \lambda v_1 + e_1 & Aw_1 = \lambda w_1 + v_1 \\ Ae_2 = \lambda e_2 & Av_2 = \lambda v_2 + e_2 \\ Ae_3 = \lambda e_3 & \end{array}$

- This is the matrix structure for one eigenvalue
- There may be more than one such blocks in general
- All matrices can be put into Jordan form
 - Matlab: jordan(A)
 - Note that the eigenvalues of J are the same as those of A

Imagine det(J - sI) = 0

$$J = TAT^{-1} = \begin{bmatrix} \lambda & 1 & 0 & & \\ 0 & \lambda & 1 & & \\ 0 & 0 & \lambda & & \\ & & & \lambda & 1 \\ & & & 0 & \lambda \\ & & & & & \lambda \end{bmatrix}$$

$$T^{-1} = \begin{bmatrix} e_1 & v_1 & w_1 & e_2 & v_2 & e_3 \end{bmatrix}$$

Functions of Matrices

- Consider a polynomial of a matrix, $f(A) = A^k$
 - $A^k = (T^{-1}JT)^k = (T^{-1}JT)(T^{-1}JT)(T^{-1}JT)...(T^{-1}JT) = T^{-1}J^kT$
 - Adjacent T matrices and inverse cancel!
- This motivates general functions of matrices, like $f(A) = \sin A$ or $f(A) = e^{At}$, defined through Taylor series

•
$$\sin A = A - \frac{A^3}{3!} + \frac{A^5}{5!} - \frac{A^7}{7!} + \cdots$$

• $e^{At} = I + \frac{At}{1!} + \frac{A^2t^2}{2!} + \cdots$

• Suppose
$$J = \begin{bmatrix} \lambda & 1 & & \\ & \lambda & \ddots & \\ & & \ddots & 1 \\ & & & \lambda \end{bmatrix} \begin{pmatrix} \uparrow & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ &$$

- And $f(A) = T^{-1}f(J)T$, where $A = T^{-1}JT$
- **Spectral theorem**: the eigenvalues of f(A) are $\{f(\lambda)\}$, where $\{\lambda\}$ are eigenvalues of A

Imagine $\det(f(J) - sI) = 0$



- Equilibrium point of $\dot{x} = f(x)$ is where f(x) = 0
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- The system $\dot{x} = Ax$ is exponentially stable if and only if all eigenvalues of A are in the open left half plane, i.e. $\forall k$, $\operatorname{Re}(\lambda_k) < 0$



LTI System: Stability

• The system $\dot{x} = Ax$ is exponentially stable if and only if all eigenvalues of A are in the open left half plane, i.e. $\forall k, \operatorname{Re}(\lambda_k) < 0$

•
$$z = Tx \Rightarrow \dot{z} = TAT^{-1}z = \Lambda z, \ z_0 = Tx_0$$

• $\begin{bmatrix} z_1(t) \\ z_2(t) \end{bmatrix} = \begin{bmatrix} e^{\lambda_1 t} & 0 \\ 0 & e^{\lambda_2 t} \end{bmatrix} \begin{bmatrix} z_{10} \\ z_{20} \end{bmatrix}$

• If $\operatorname{Re}(\lambda_k) < 0$, $e^{\lambda_k t} \to 0$, so $z_k(t) = e^{\lambda_k t} z_{k0} \to 0$



• If max $\operatorname{Re}(\lambda_k) = 0$, z(t) stays bounded only if $\overline{\lambda}_k$ has Jordan block of size 1

Eigenvalue with largest real part

LTI System: Stability

- If max $\operatorname{Re}(\lambda_k) = 0$, z(t) stays bounded only if $\overline{\lambda}_k$ has Jordan block of size 1
- $e^{Jt}z_{0} = \begin{bmatrix} e^{\lambda_{1}t} & & & \\ & e^{\lambda_{1}t} & te^{\lambda_{1}t} & & \\ & & e^{\lambda_{1}t} & & \\ & & & e^{\lambda_{2}t} & te^{\lambda_{2}t} & \frac{1}{2}t^{2}e^{\lambda_{2}t} \\ & & & & e^{\lambda_{2}t} & te^{\lambda_{2}t} \\ & & & & & e^{\lambda_{2}t} & te^{\lambda_{2}t} \\ & & & & & e^{\lambda_{2}t} \end{bmatrix} z_{0}$ • When $\lambda_i = 0$...

LTI System: Stability

• If max $\operatorname{Re}(\lambda_k) = 0$, z(t) stays bounded only if $\overline{\lambda}_k$ has Jordan block of size 1

$$e^{Jt}z_{0} = \begin{bmatrix} 1 & & & & \\ & 1 & t & & \\ & & 1 & & \\ & & & 1 & t & \frac{1}{2}t^{2} \\ & & & & 1 & t \\ & & & & 1 & t \\ & & & & & 1 \end{bmatrix} z_{0}$$

- When $\lambda_i = 0$...
- Not stable!

State Feedback Control

- Suppose $\dot{x} = Ax + Bu$, can we design u to make $x = \mathbf{0}_n$ stable?
- Try linear state feedback: $u = -Kx \Rightarrow \dot{x} = (A BK)x$
 - Define $\overline{A} = A BK$, and we have $\dot{x} = \overline{A}x$
 - We can try to choose the elements of K, such that the eigenvalues of A
 are in the left half-plane



Stabilization by State Feedback

- Suppose $\dot{x} = Ax + Bu$, where $A = \begin{bmatrix} 2 & 2 \\ 0 & 2 \end{bmatrix}$, $B = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$
 - Is the system stable when $u(t) \equiv 0$? No!

•
$$Ax = \lambda x \Rightarrow (A - \lambda I)x = 0$$

• det
$$\begin{pmatrix} 2-\lambda & 1\\ 0 & 2-\lambda \end{pmatrix} = 0 \Rightarrow \lambda = 2,2$$

- Choose K so that u = -Kx stabilizes the system.
 - Let $K = \begin{bmatrix} k_1 & k_2 \end{bmatrix}$, then $\bar{A} \coloneqq A BK = \begin{bmatrix} 2 k_1 & 2 k_2 \\ -k_1 & 2 k_2 \end{bmatrix}$
 - det $(\bar{A} \lambda I) = (2 k_1 \lambda)(2 k_2 \lambda) + (2 k_2)k_1$
 - Choose k_1 , k_2 such that $det(\bar{A} \lambda I) = 0$ gives λ in the open left half plane

Stabilization by State Feedback

- Choose K so that u = -Kx stabilizes the system.
 - Let $K = \begin{bmatrix} k_1 & k_2 \end{bmatrix}$, then $\bar{A} \coloneqq A BK = \begin{bmatrix} 2 k_1 & 1 k_2 \\ 1 k_1 & 2 k_2 \end{bmatrix}$ • $0 = (2 - k_1 - \lambda)(2 - k_2 - \lambda) + (2 - k_2)k_1$ • $0 = \lambda^2 + (k_1 + k_2 - 4)\lambda + (2 - k_1)(2 - k_2) + (2 - k_2)k_1$ • $0 = \lambda^2 + (k_1 + k_2 - 4)\lambda + 4 - 2k_1 - 2k_2 + k_1k_2 + 2k_1 - k_1k_2$ • $0 = \lambda^2 + (k_1 + k_2 - 4)\lambda + 4 - 2k_2$
- One choice: $\lambda = -2, -2$
 - $0 = (\lambda + 2)(\lambda + 2) = \lambda^2 + 4\lambda + 4$
 - $k_2 = 0, k_1 = 8$

State Feedback Control

- Suppose $\dot{x} = Ax + Bu$, can we design u to make $x = \mathbf{0}_n$ stable?
- Try linear state feedback: $u = -Kx \Rightarrow \dot{x} = (A BK)x$
 - Define $\overline{A} = A BK$, and we have $\dot{x} = \overline{A}x$
 - We can try to choose the elements of K, such that the eigenvalues of \overline{A} are in the left half-plane
- Issues
 - Controller saturation
 - Full state information required